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Better models for better engines: towards multi-physics modelling

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Free University of Bozen, 12/13/2018



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Outline

1. Introduction

- The University of Wisconsin Engine Research Center
- Why study combustion in 2018?

2. Multidimensional modelling of internal combustion engines

- Modeling approaches to ICEs: 0D, 1D
- 3D modelling: history
- In-cylinder flow and turbulence modelling

3. Multi-physics models for engines: examples

- Combustion: chemical kinetics modelling and flame propagation
- Spray: breakup and vaporization

4. Conclusions/Outlook



Engine Research Center

www.erc.wisc.edu



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University of Wisconsin- Madison

- Founded in 1848
- 29,536 undergraduate / 8,904 graduate students
- 2,200 faculty
- Nearly \$1 billion/year in research funding
- No. 2 ranking among all US public universities



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UW-Madison



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Consultants

UW-Madison College of Engineering

- 5000 undergraduate students
- 1600 graduate students
- 180 faculty
- \$150M/year in research funding
- More than \$80 million annually in energy research
 - Fusion: \$15 million per year
 - Fission: \$5 million per year
 - Biofuels: \$28 million per year
 - Automotive: \$5 million per year



UW-Madison: Mechanical Engineering

- 850 undergraduate students
- 225 graduate students
- 30 faculty
- \$10M/year in research funding



Brief ERC History

- The Engine Research Center (ERC) was established in 1946 by Profs. Myers and Uyehara, who were joined by Prof. Borman in 1970.
- 1986 – ERC was designated a Center of Excellence by the Army Research Office
- Over the 70 years of its existence, the ERC has pioneered:
 - in-cylinder measurements of gas temperature, composition and heat flux
 - the simulation of turbulent, multi-phase, reacting flows in reciprocating engines
 - high efficiency, low-emissions combustion strategies such as RCCI and HCCI



Engine Research Center

Founded in 1946

ARO Center of Excellence; DOD

DOE; Consortia/Industry



Myers Uyehara Borman

1985 - 2003



Chris Rutland



Jaal Ghandhi



Scott Sanders



Mario Trujillo



David Rothamer

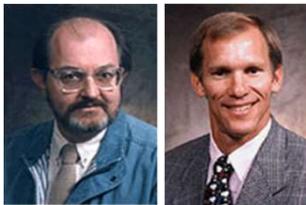


Sage Kokjohn

2003 +

2-color soot radiation, droplet experiments

0-D engine simulation, heat release analysis



Rolf Reitz Dave Foster

First to demonstrate HCCI in a 4-stroke engine

First to demonstrate benefits of multiple injections for power and emissions

Pioneered Multi-Dimensional modeling for concept evaluation

Advanced spray/combustion diagnostics for fuel-air mixing and emissions characterization

In-cylinder gaseous species measurement, high resolution spray analysis

High-fidelity engine codes, detailed chemistry for emission prediction, spray & turbulence modeling

Control strategies

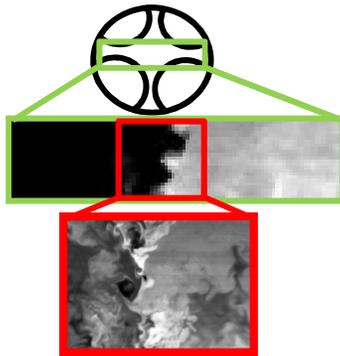
Combustion system optimization

Aftertreatment experiments and modeling

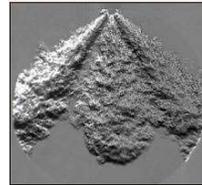


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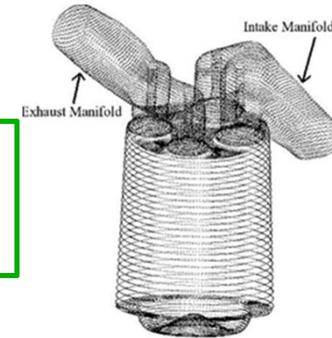
ERC Research Projects



Fuel Injection and Sprays



Combustion Optimization and Emissions



Charge Preparation

Low Emissions High Efficiency

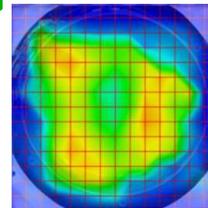


The logo of the Engine Research Center at the University of Wisconsin-Madison, established in 1946. It features a stylized engine and the text 'ENGINE RESEARCH CENTER UNIVERSITY OF WISCONSIN-MADISON EST 1946'.

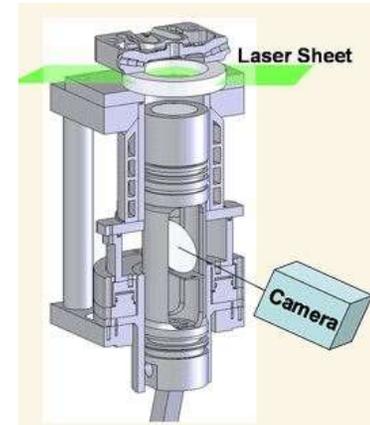
Exhaust Aftertreatment



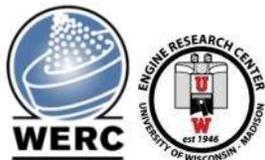
Controls



Diagnostics



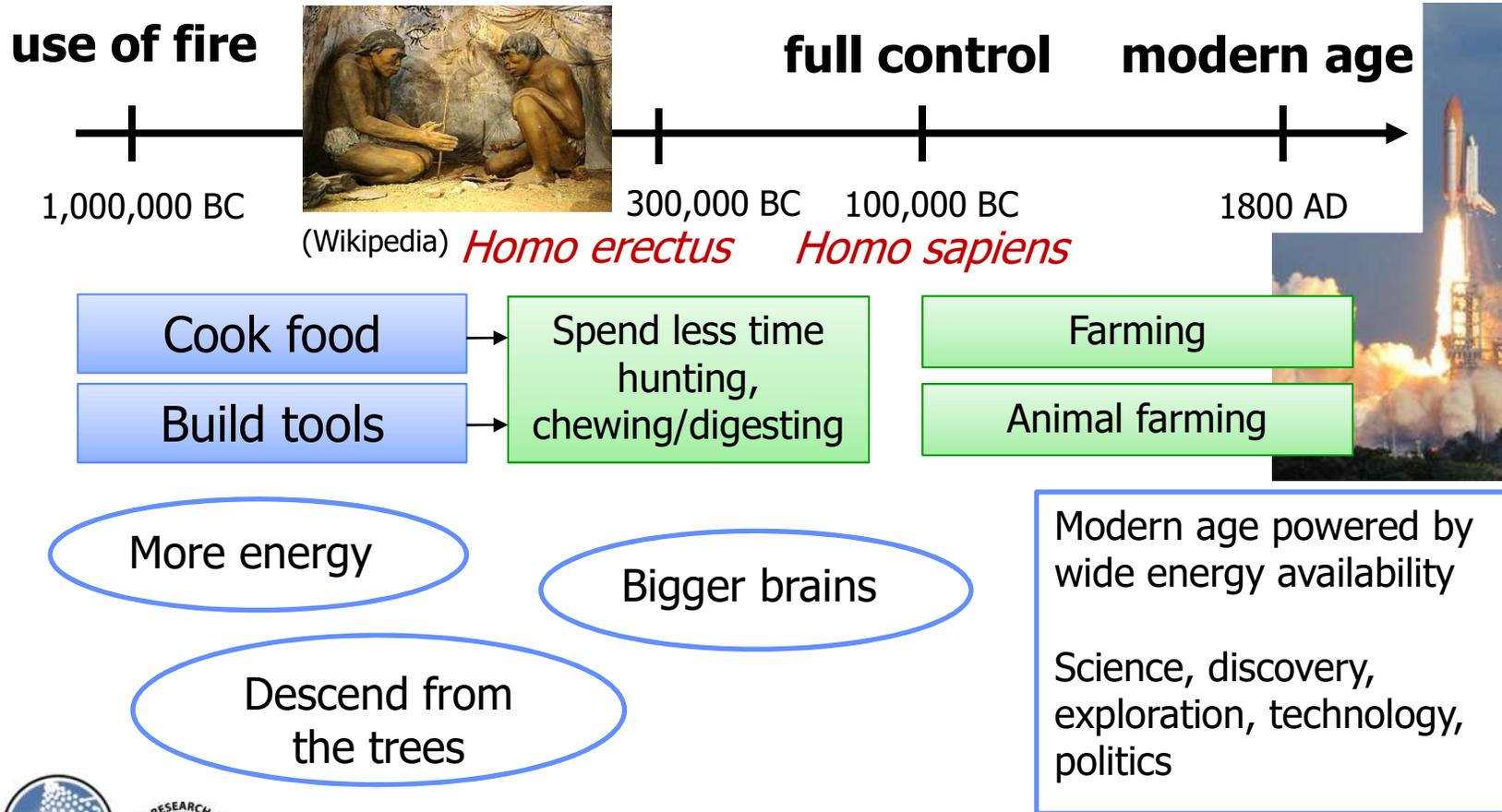
1. introduction



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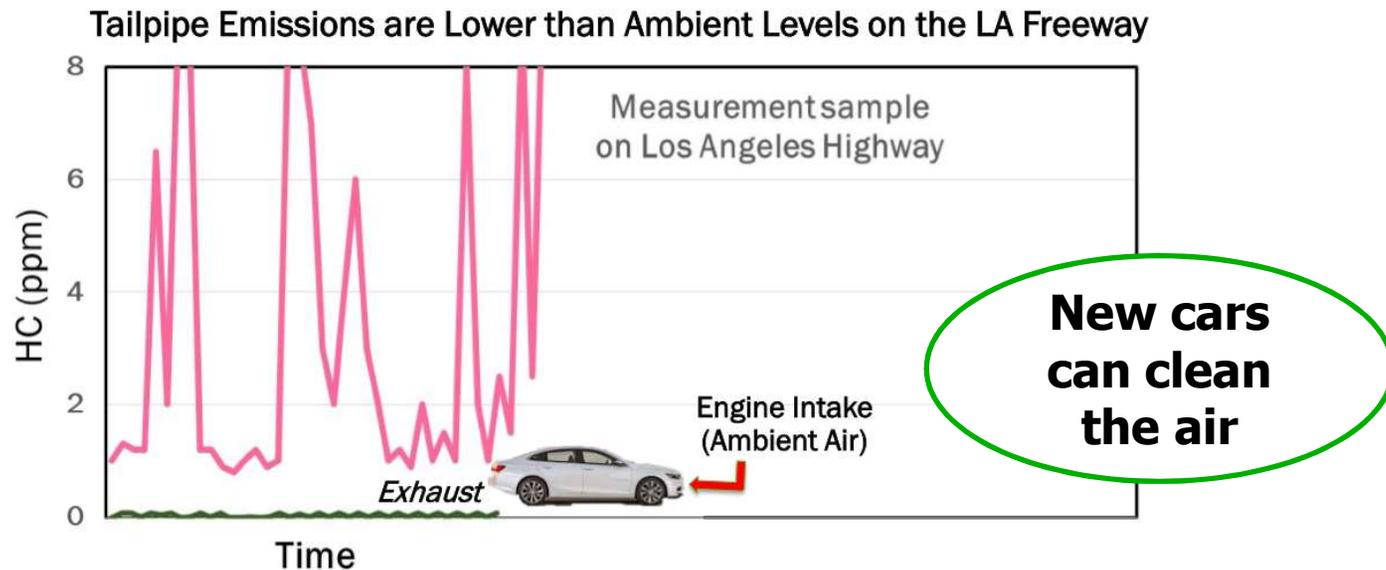
Why study combustion in 2018?

For 10,000 centuries, combustion has made our development as humans possible.



Why study combustion engines?

- Environmental pollution of IC engines reduced by more than 99% during the last 30 years
- Currently the least among alternatives (e.g., BEV)
 - battery electric engines move pollution to a different location (power station)
 - utilization of scarce natural resources & labor exploitation



NOTE: Curves replotted to approximate Figure 1 curves of source document. Source: Johnson, T. and Joshi, A., "Review of Vehicle Engine Efficiency and Emissions," SAE Technical Paper 2018-01-0329, 2018, doi:10.4271/2018-01-0329.

Why study combustion engines?

- **Concern due to fossil fuel combustion causing global warming / climate change**
- **Fuel economy ~doubled since 1980 despite ~20% heavier vehicles**

| Program Area | Annual Petroleum Savings (million bpd) | | | Annual Emissions Reduction (million tons CO _{2e}) | | |
|--|---|------------------|------------------|--|----------------|----------------|
| | 2025 | 2035 | 2050 | 2025 | 2035 | 2050 |
| Electrification | 0.03-0.19 | 0.28-0.61 | 0.34-1.44 | 5-29 | 57-123 | 74-272 |
| Advanced Combustion Engines and Fuels | 0.25-0.32 | 0.66-1.01 | 0.85-1.01 | 47-62 | 122-194 | 151-182 |
| Materials Technology | 0.02-0.03 | 0.06-0.12 | 0.06-0.08 | 4-7 | 11-24 | 11-15 |
| Hydrogen Fuel Cells | 0.00-0.05 | 0.11-0.45 | 0.35-0.96 | 0-6 | 14-46 | 59-148 |

U.S. efforts estimate that benefits due to advanced combustion technologies will equal or even outperform those of electrification in the next 30 years

Source: Stephens, et al. (2017), Vehicle Technologies and Fuel Cell Technologies Office Research and Development Programs: Prospective Benefits Assessment Report for FY 2018.
<http://www.ipd.anl.gov/anlpubs/2017/11/140256.pdf>

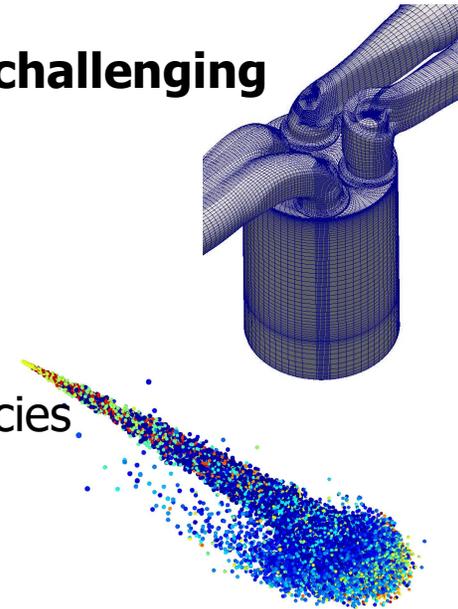


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Co-Design of Engines and Fuels will be enabled by computing

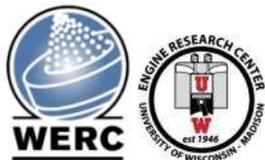
■ Accurate simulation of engine combustion is challenging

- Complex geometries with moving boundaries
- Turbulence models are lacking
- Multi-phase reacting sprays
- Ability to model real fuels: 1000+ chemical species
- Time-scales: 10^{-9} s to 1 s
- Length scales: 10^{-6} m to 10^{-2} m



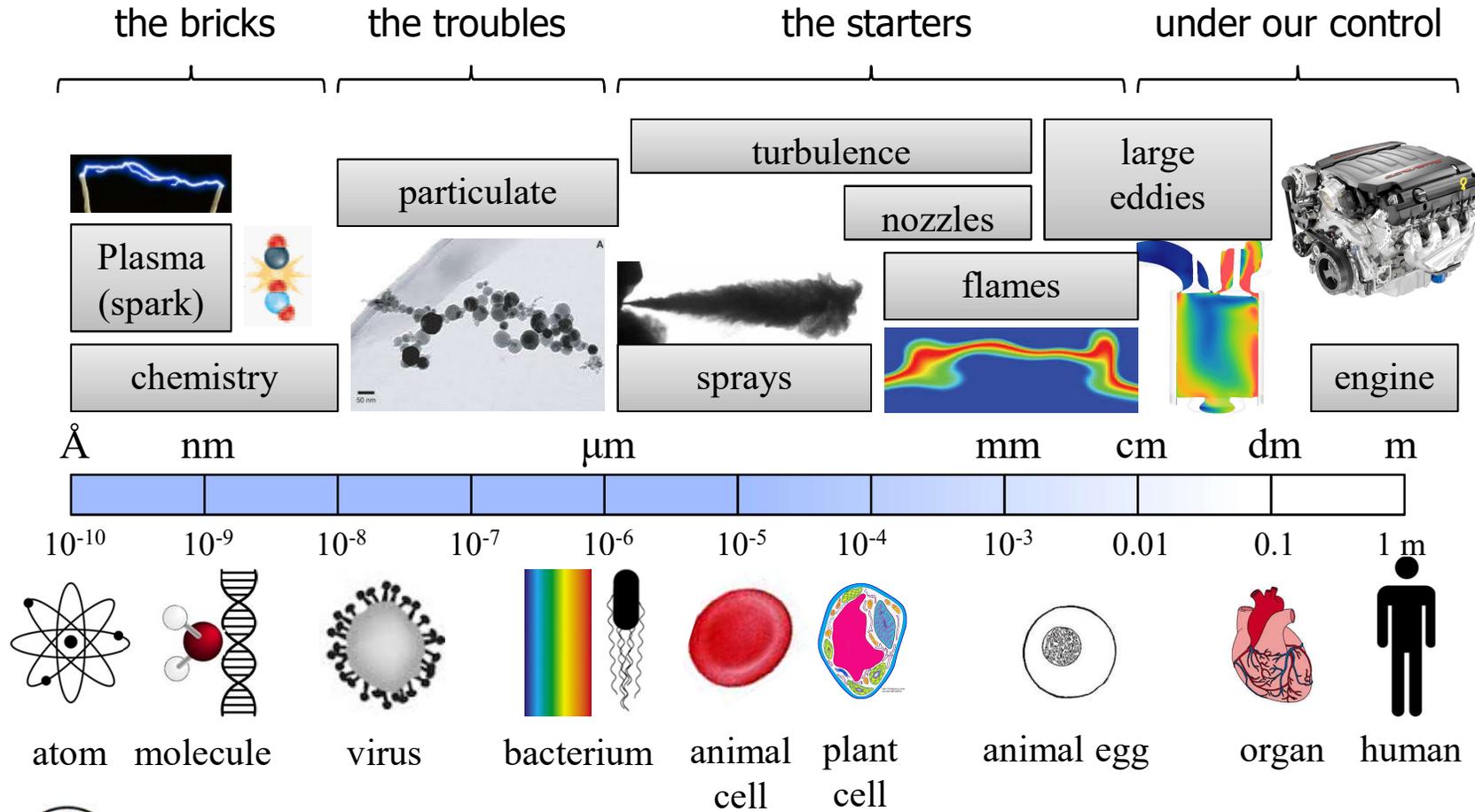
Developing scalable, accurate codes with multi-physics models to accelerate engine combustion research

Source: Gupreet Singh (2018), Overview: Advanced Combustion Systems and Fuels R&D,
https://www.energy.gov/sites/prod/files/2018/06/f53/acs918_singh_2018.pdf

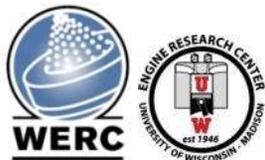


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ICE phenomena vs. biological scales



At least 8 orders of magnitude fit into the same model



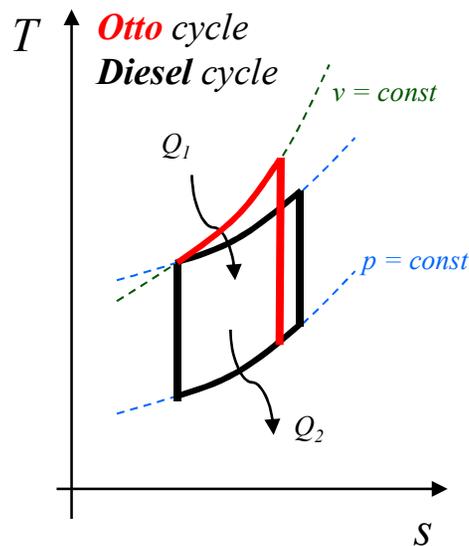
2. Internal combustion engine modelling



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0D and 1D engine modelling

- Engine combustion happens somewhere between constant-pressure and constant-volume



Perini et al., 2010

1st Law of Thermodynamics

$$d\dot{U} = \delta\dot{Q} - d\dot{W}$$

fuel → walls → shaft

$$mc_v \frac{dT}{dt} + p \frac{dV}{dt} + \sum_j \dot{m}_j h_j = q_{comb} - q_{wall}$$

Ideal gas EoS
closes p,V
relationship

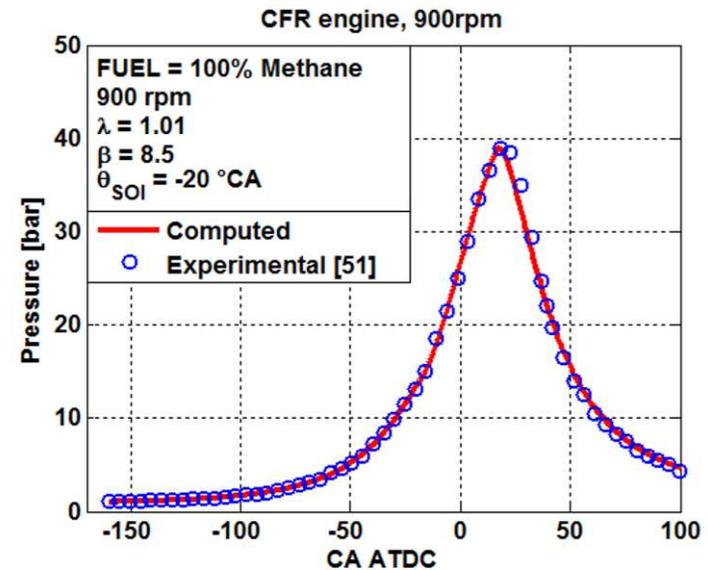
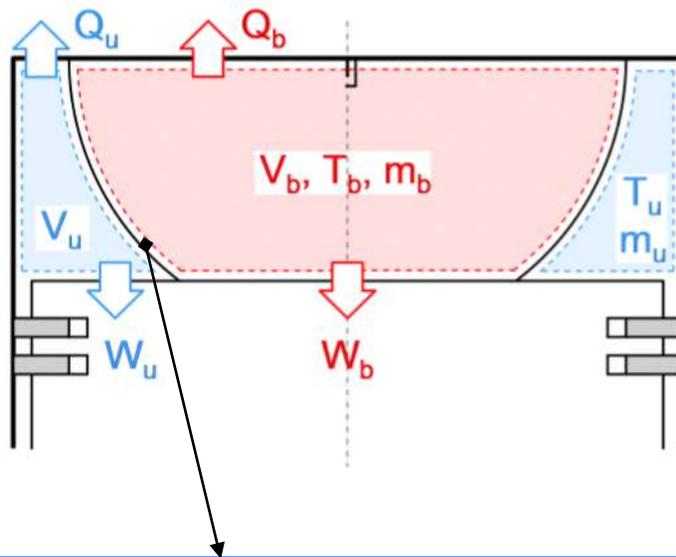
Combustion
model

Heat transfer
 $q_w = hA(T - T_w)$



0D and 1D engine modelling

- The whole cylinder or a finite number of "zones" are used as **control volumes**



Flame propagation modelling

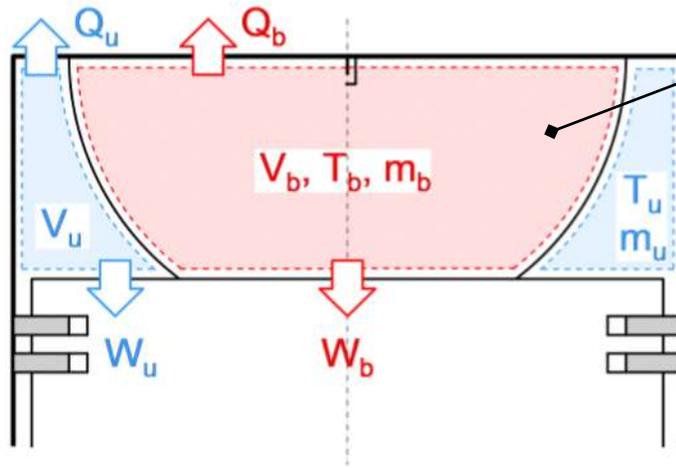
$$s_L = s_L(\phi, p, T, f_{res}) = S_{L,0} \left(\frac{T}{T_0}\right)^\alpha \left(\frac{p}{p_0}\right)^\beta (1 - \gamma f_{res})$$

Perini et al., 2010

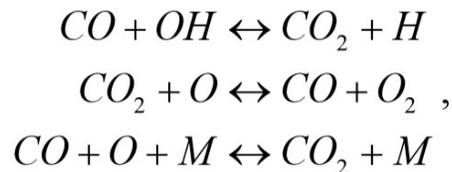


0D and 1D engine modelling

- The whole cylinder or a finite number of "zones" are used as **control volumes**

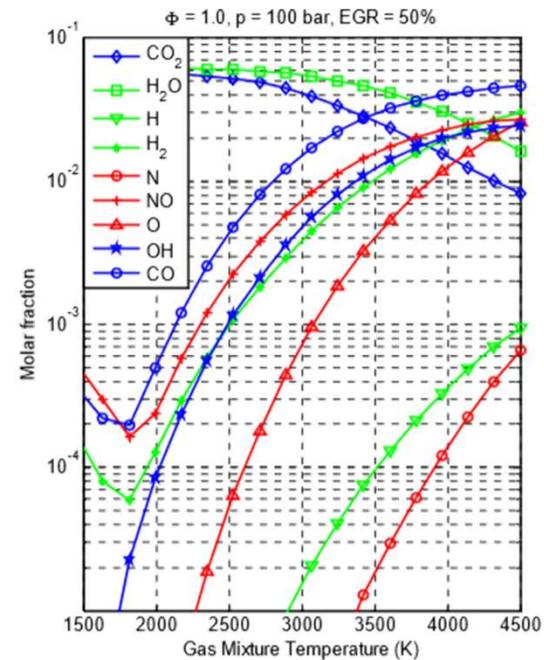


Simple kinetics laws on top of the equilibrium radical pool



Pollutant formation modelling

Assume chemical equilibrium in the burnt zone



Perini et al., 2011

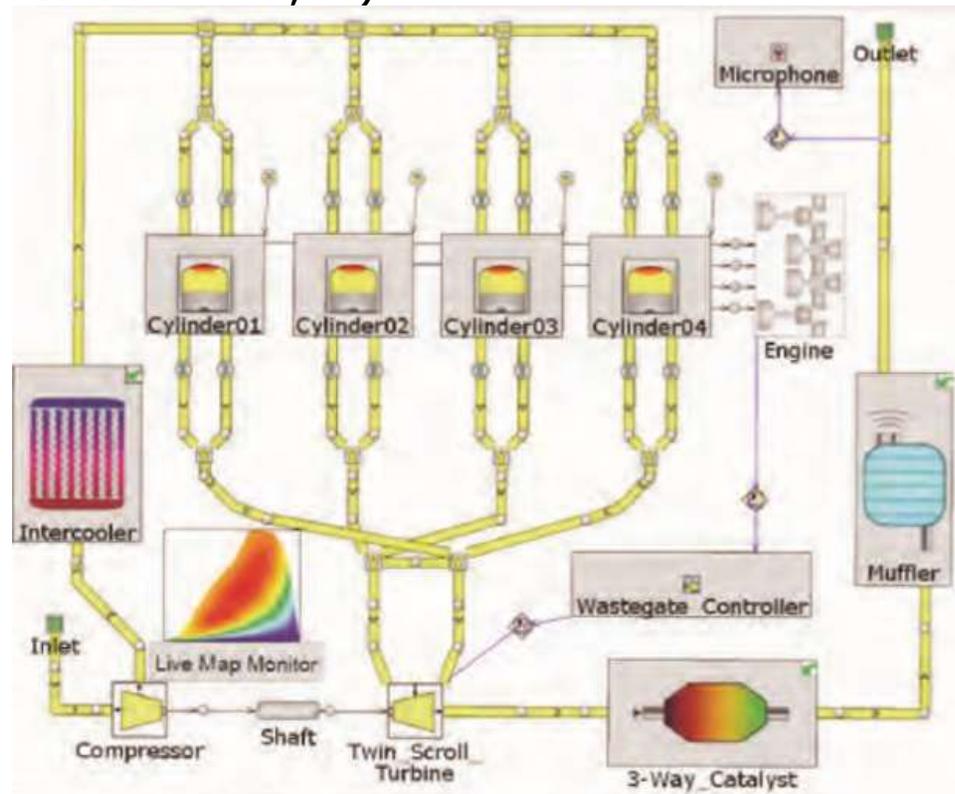
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1D engine modelling

- **0D models for the cylinder and other systems are bound with pipe systems into 1D modelling codes**
(GT-Power, AVL-Boost, Ricardo WAVE, ...)

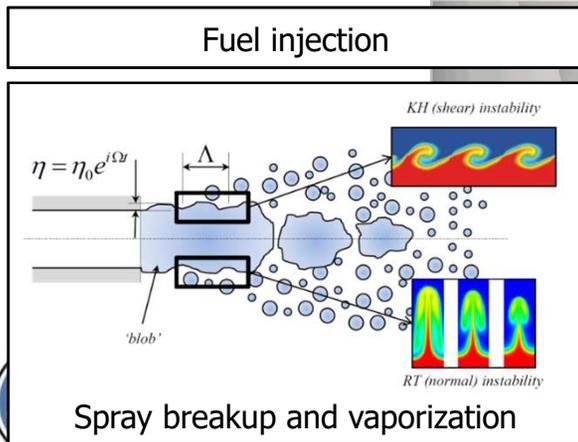
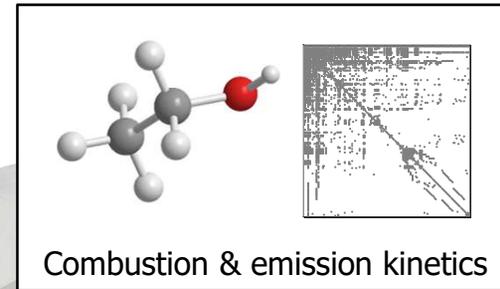
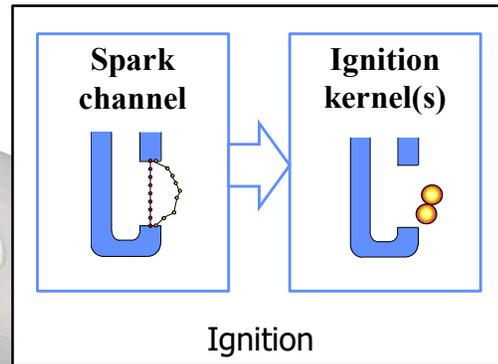
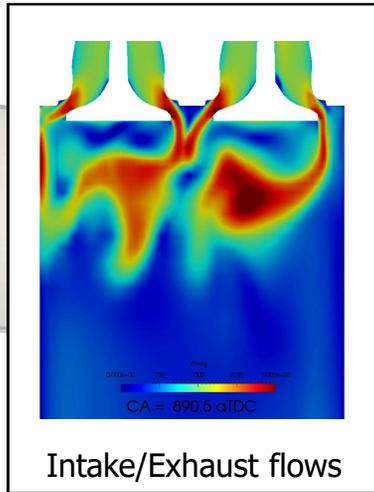
- Model pressure oscillations and inertia of flowing gases to capture correct engine breathing

- System-level operation:
 - Valve timing
 - Exhaust temperature control
 - In-cylinder EGR

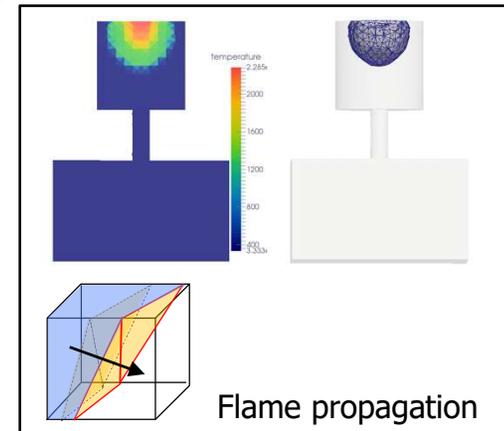


3D engine modelling

Multi-physics approach



Fluid Mechanics
Turbulence
Wall heat transfer
Crevice flows



3D engine modelling

A brief history

Arab oil crisis circa 1973: US DOE

■ Open-source codes

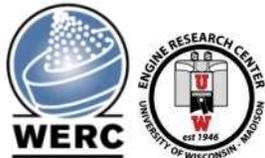
- Los Alamos National Lab, Princeton University, UW-ERC
- 1970's – RICE → REC → APACHI → CONCHAS
- 1980's CONCHAS-SPRAY → KIVA family
- 1985 – KIVA; 1989 – KIVA-II; 1993 – KIVA-3
- 1997 – KIVA-3v; 1999 – KIVA-3v Release 2; 2006 – KIVA-4
- 2004 – OpenFOAM (2011 SGI) (2012 ESI group)

■ Commercial codes

- 1980's Imperial College London & others
- Computational Dynamics, Ltd. → STAR-CD
- 1990's other commercial codes: AVL-FIRE, Ricardo VECTIS
- 2005 – FLUENT (with moving piston and cylinder models)
- 2010 – CONVERGE (CSI), FORTE (ANSYS)
- 2018 – FRESCO (WERC)



Annual IMEM-User Group Meeting: UW-ERC/MTU
SAE Multidimensional Modeling sessions, ASME, ...



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3D-CFD model equations

- Solve conservation equations on a moving finite-volume mesh

mass

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = \dot{\rho}_s$$

species

$$\frac{\partial \rho_m}{\partial t} + \nabla \cdot (\rho_m \mathbf{u}) = \nabla \cdot \left[\rho D_t \nabla \left(\frac{\rho_m}{\rho} \right) \right] + \dot{\rho}_m^c + \dot{\rho}_m^s$$

momentum

$$\frac{\partial (\rho \mathbf{u})}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u}) = -\nabla p + \nabla \cdot \bar{\bar{\sigma}} + \rho \mathbf{g} + \mathbf{F}^S$$

energy

$$\frac{\partial (\rho I)}{\partial t} + \nabla \cdot (\rho \mathbf{u} I) = -\nabla \cdot \mathbf{J} + \dot{Q}_c + \dot{Q}_s - p \nabla \cdot \mathbf{u} + \bar{\bar{\sigma}} : \nabla \mathbf{u}$$

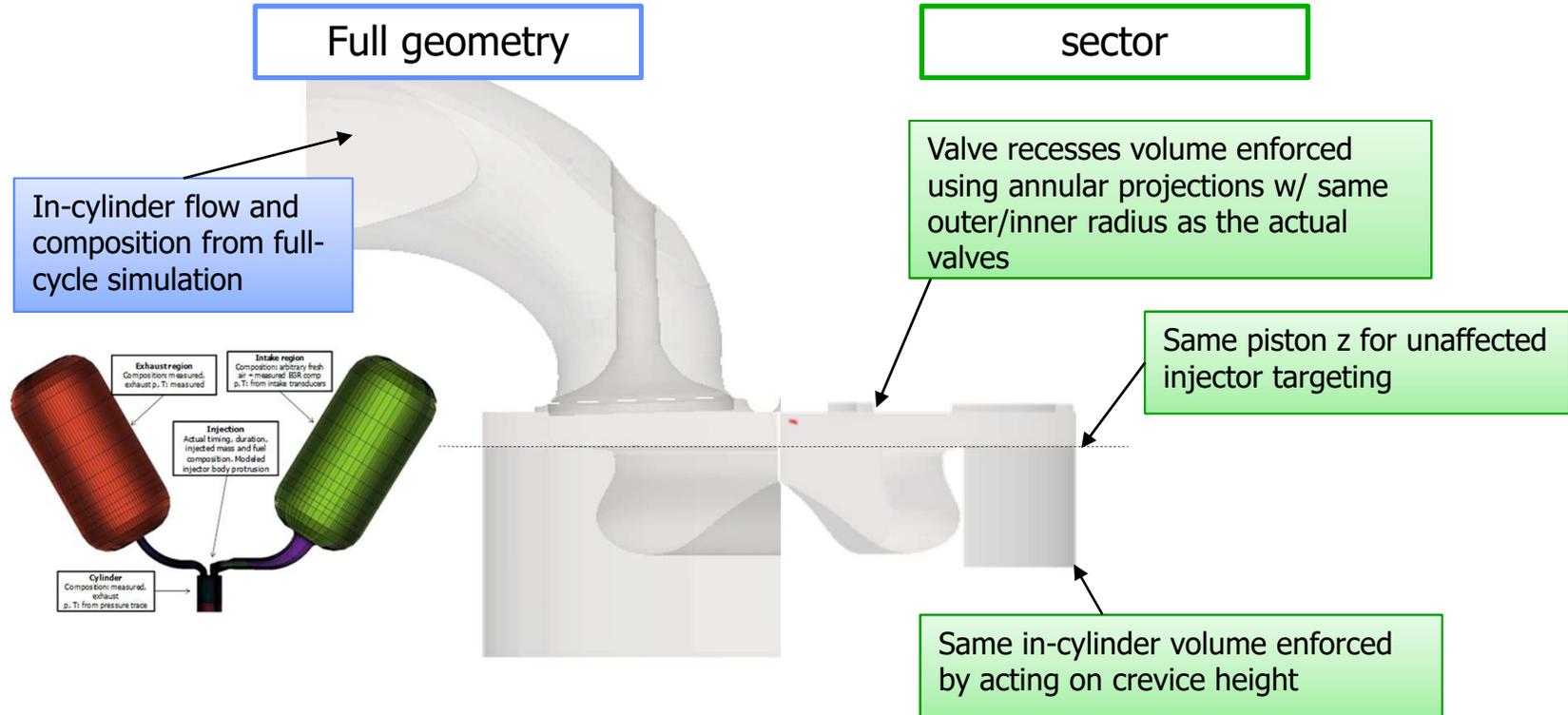
$s = \text{spray}$
 $c = \text{combustion}$



Torres, Trujillo 2006

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3D engine modelling approaches



- Symmetric swirling flow imposed
- Thermodynamic state (p , T , composition) and turbulence are cylinder-averaged quantities

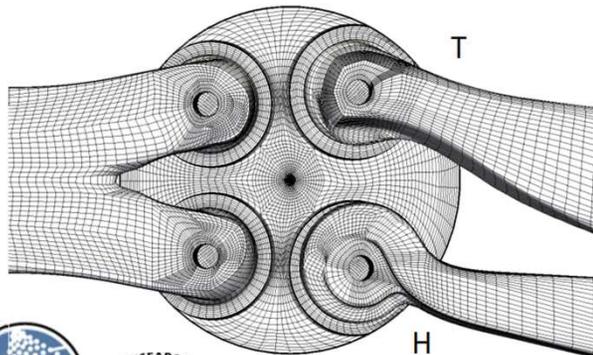
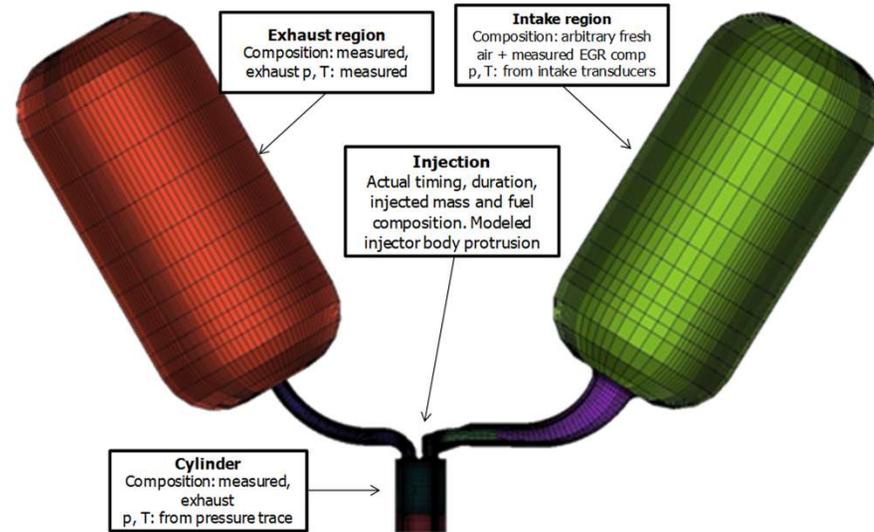


Perini, SAE2019

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In-cylinder flow modelling

| Engine configuration | |
|---------------------------|--|
| Compression ratio | 16.1 : 1 |
| Squish height at TDC [mm] | 1.36 |
| Piston bowl geometry | Stepped-lip |
| Operating conditions | |
| Engine speed [rev/min] | 1500 |
| Intake pressure [bar] | 1.5 |
| Intake temperature [K] | 372 |
| Swirl Ratio (Ricardo) [-] | 2.2 |
| Intake charge [mol fr.] | 10% O ₂ , 81% N ₂ , 9% CO ₂ |
| FRESCO solver setup | |
| mesh accuracy | Body-fitted, unstructured hexa |
| time accuracy: | hybrid 1st-order implicit (diffusion, momentum) / explicit (advection) |
| spatial accuracy: | 2nd-order (diffusion) upwind (advection) |

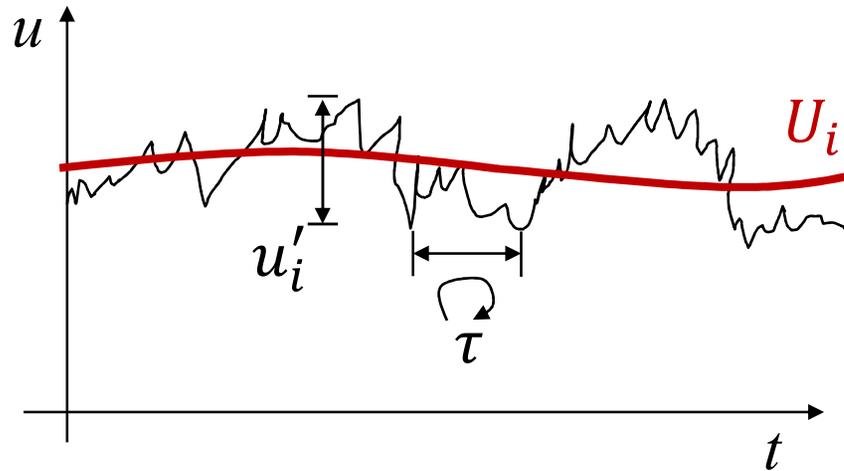


- Flow configuration from moderately-boosted, low-load operating condition ("LTC3")
- Experimental PIV measurement campaign provides ensemble-averaged flow structure at in-cylinder horizontal plane locations during the intake and compression strokes
- $dz = 3.0, 10.0, 18.0$ mm from fire-deck



Flow and turbulence modelling in engines

Turbulence closure



$$u_i = U_i + u'_i$$

Sub-grid velocity

RANS: ensemble (Favre) filtering

LES: spatial filtering

- Boussinesq assumption: linear stress-strain closure

Mean flow strain rate

$$S_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

Reynolds stress tensor

$$\boldsymbol{\tau} = 2\mu_t \mathbf{S} - \frac{2}{3} \rho k \delta_{ij}$$

tke production

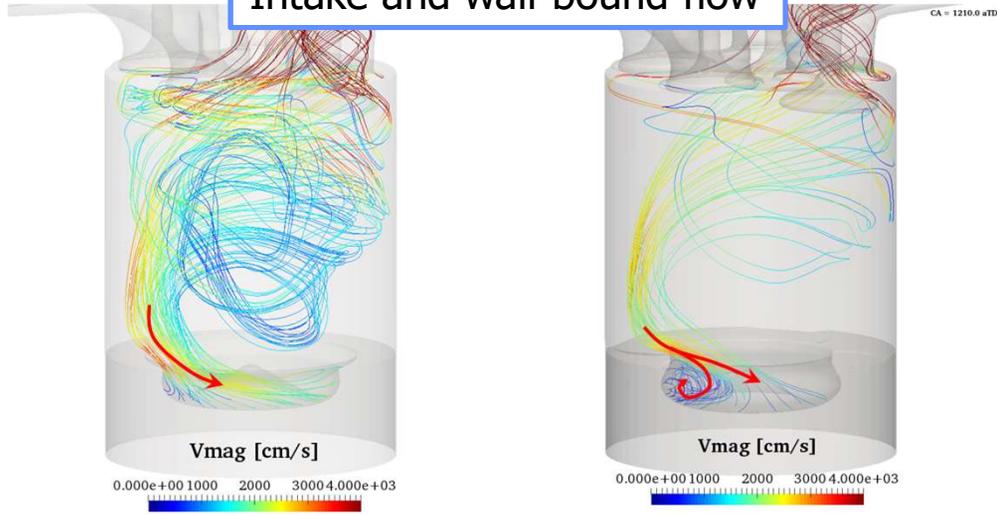
$$P = -\boldsymbol{\tau} : \nabla \mathbf{u}$$



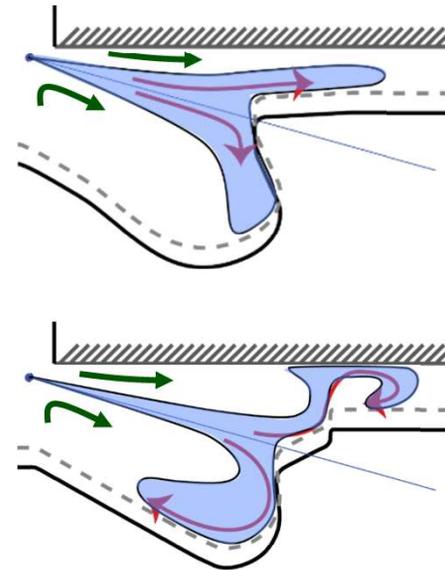
Flow and turbulence modelling in engines

Turbulence generation mechanisms

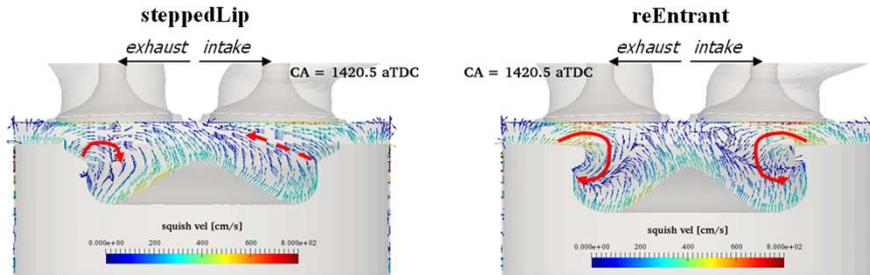
Intake and wall-bound flow



Gas jets



Squish-swirl interaction



Entrainment

Jet-wall interaction

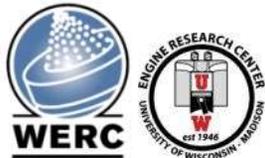


Perini et al., 2017

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Multi-physics models for engines

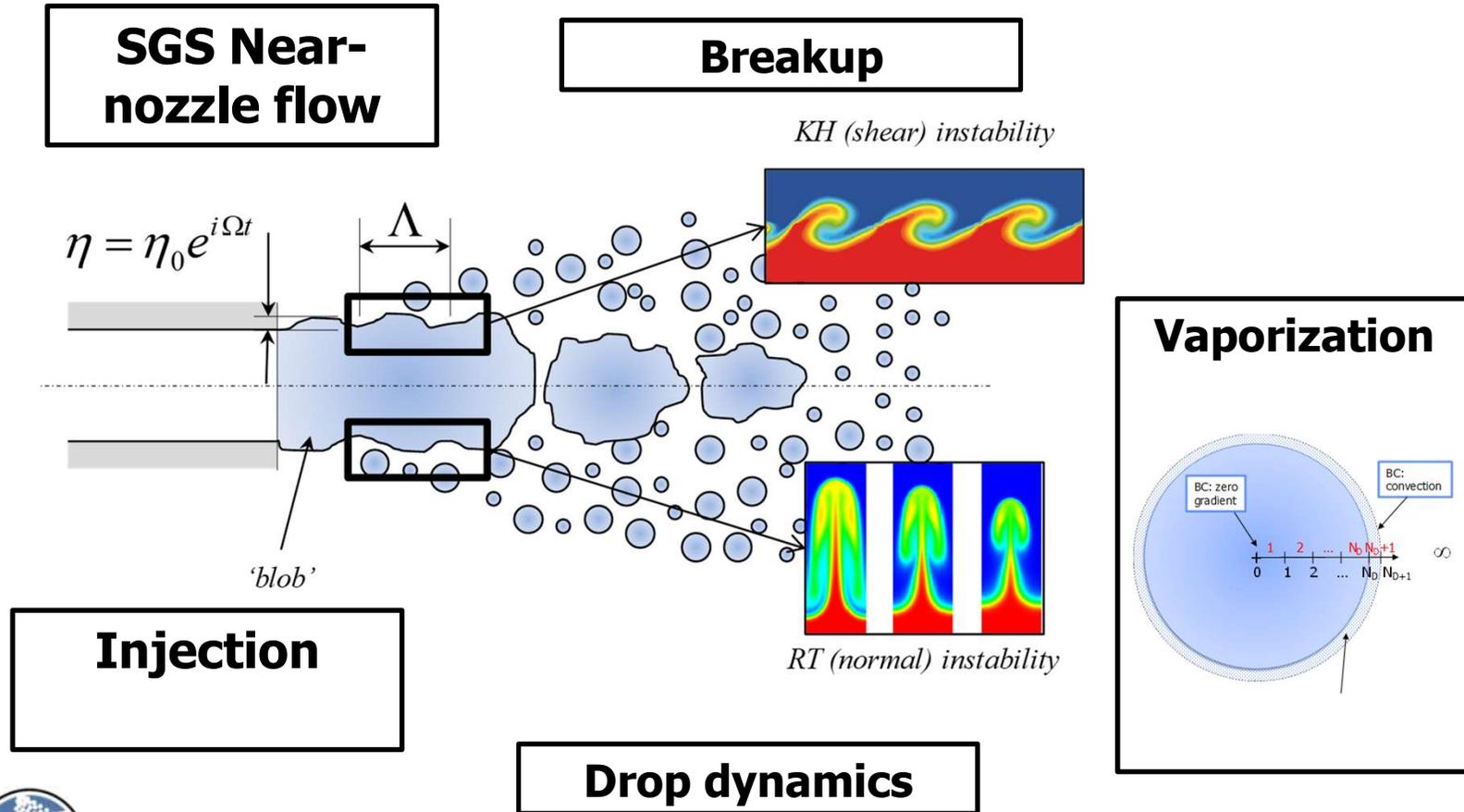
Spray modelling



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LDEF spray modelling

- Lagrangian-Drop/Eulerian-Fluid approach (LDEF)
- the liquid phase is a moving **mass, momentum, energy source terms** for the gas phase

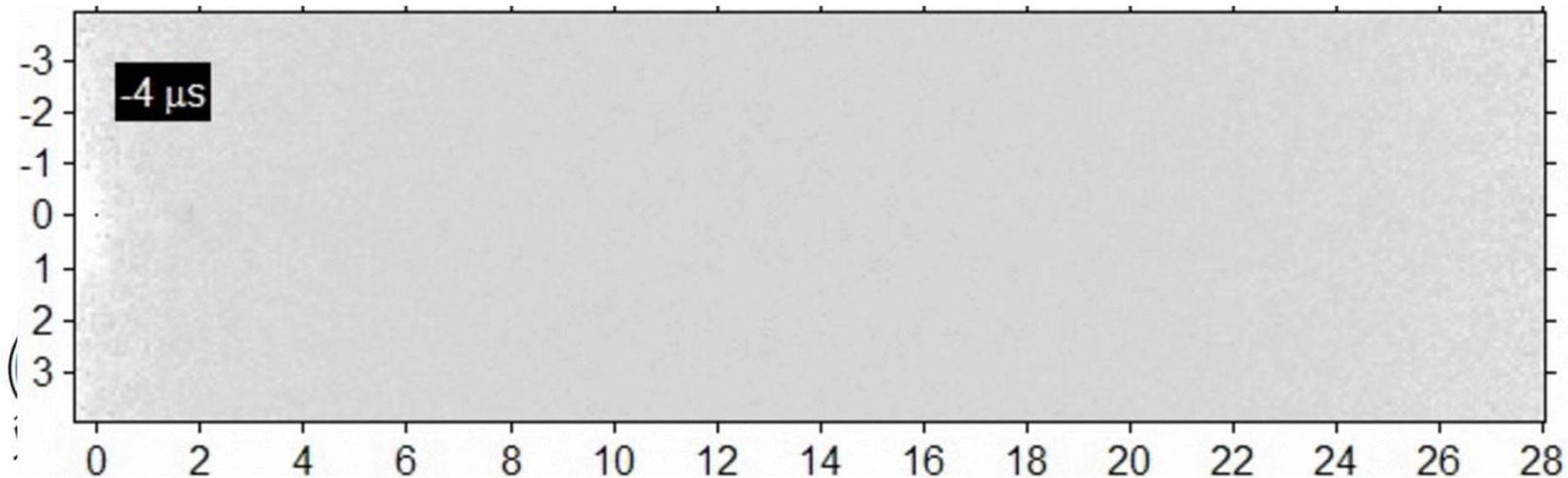
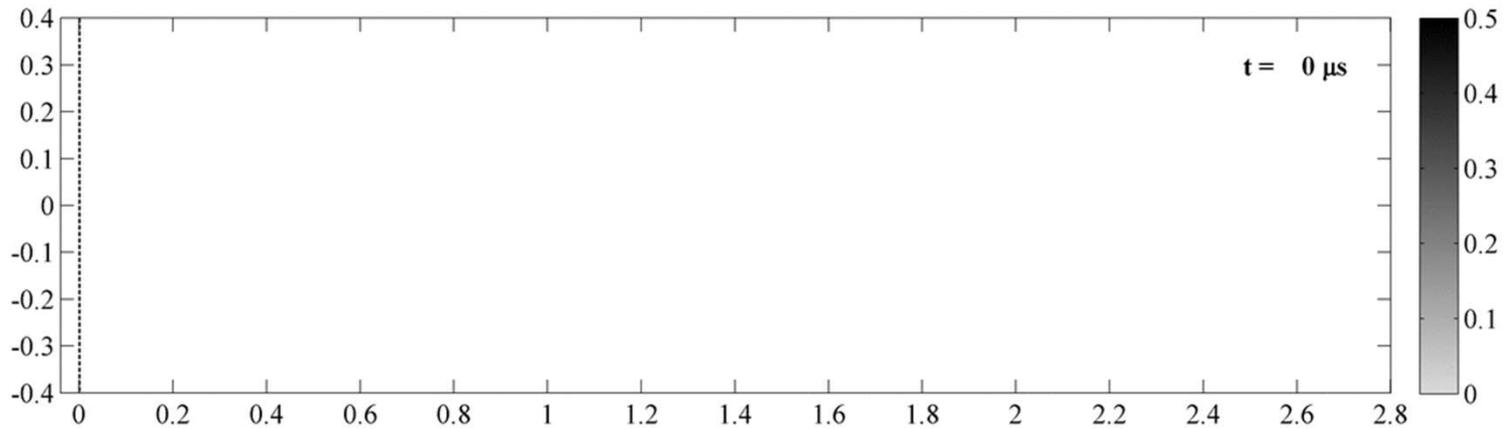


Sandia Spray A

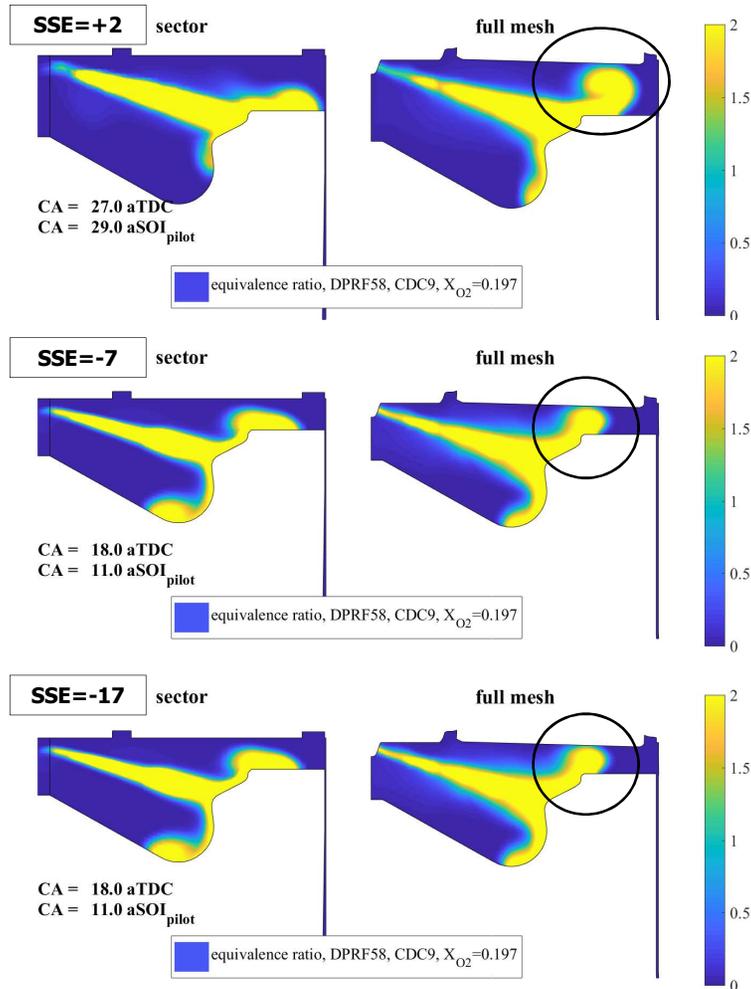
Perini, IJMF 2016

Manin, 2012

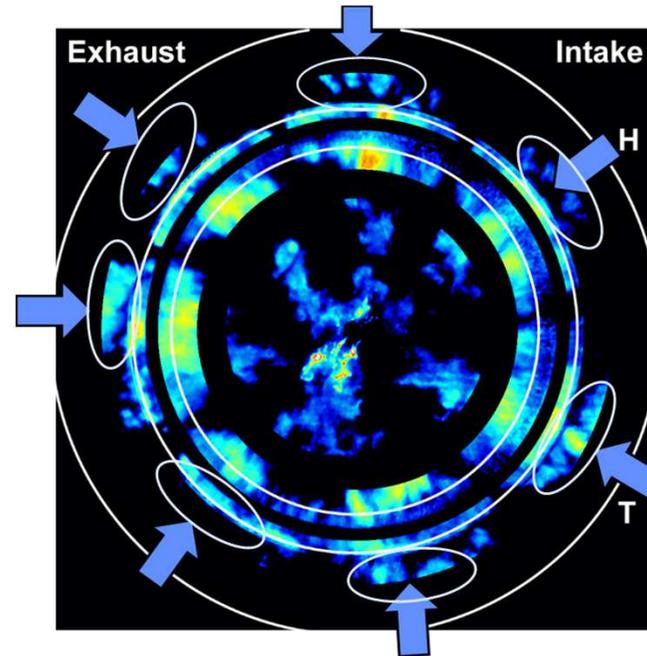
- Fuel-air mixing in the transcritical regime presents mixed liquid spray dynamics and miscible mixing phenomena



Local turbulence affects mixing



- Flow separation crucial to air utilization mechanism
- Happens regardless of injection timing
- **Never** captured by sector approach



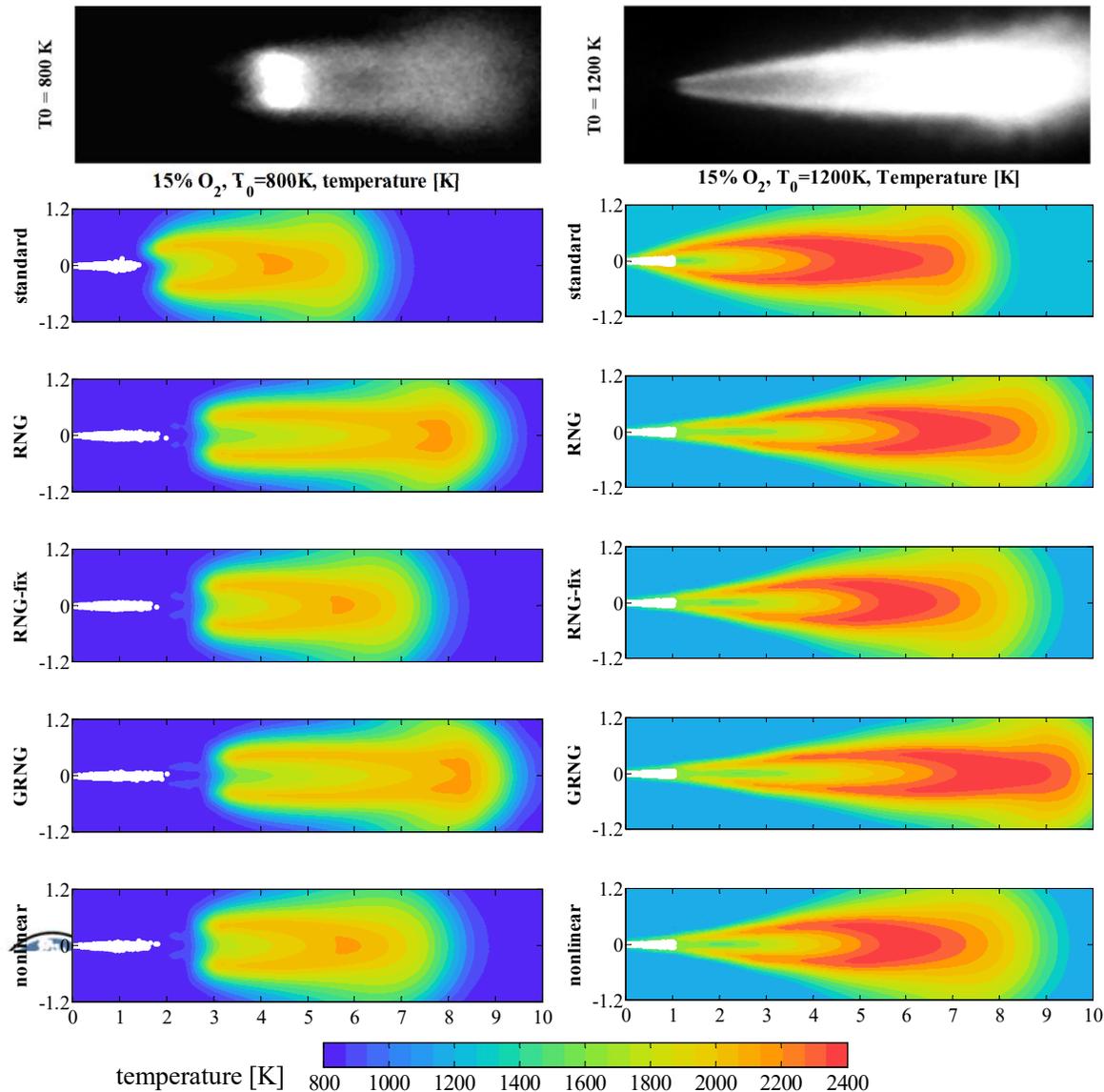
- Fuel tracer PLIF (LTC) at 12 aSOI. Same encroachment of fuel from the outer regions of the squish region.



Perini et al., 2019

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Mixture formation defines combustion and pollutant formation



RNG and GRNG

- Less radial dispersion
- Deeper penetration
- 'Bubbly' flame tip structure at $z > 8\text{ cm}$

RNG-fix and non-linear

- Similar radial dispersion
- High-temperature LOL still immediately downstream of the liquid jet
- No bubbly structure

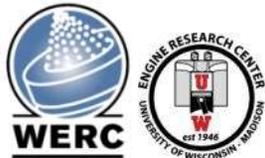
Standard k-epsilon

- LOL way upstream of any other models
- High-T LOL happens inside the liquid jet \rightarrow excessive air entrainment

\rightarrow Incorrect gas jet structure adds up with temperature and compositional gradients

Multi-physics models for engines

Combustion



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Chemical Kinetics in CFD simulations

- Usually part of an operator-splitting scheme
- Each cell is treated as an adiabatic well-stirred reactor
 - “Embarassingly” parallel problem
 - Very stiff ODE system ← need for appropriate integrators
 - Only the overall changes in species mass fractions and cell internal energy are passed to the flow solver

Skeletal mechanism or on-the-fly reduction

Reduce number of integrations

→ storage/retrieval, multi-zone approaches, clustering

$$\bullet \frac{\partial Y_i}{\partial t} = -\nabla \cdot (Y_i \mathbf{v}) - \nabla \cdot Y_i \mathbf{v}_{d,i} + \frac{1}{\rho} \dot{\omega}_i W_i$$

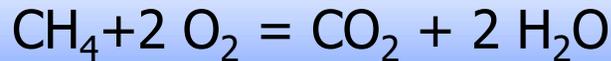
$$\bullet \frac{\partial E}{\partial t} = -\nabla \cdot (E \mathbf{v}) - \nabla \cdot (\mathbf{v} \cdot \mathbf{T}) - \nabla \cdot (\dot{Q} + \dot{Q}_r) + \mathbf{v} \cdot \sum_j m_j \mathbf{a}_j + \sum_j \mathbf{v}_{d,i} \cdot m_j \mathbf{a}_j$$



Combustion reaction mechanisms

■ CH₄ reaction mechanism: 15 species, 30 reactions

Warnatz, 2006



Methane consumption

1. $\text{CH}_4 + \text{H} \rightleftharpoons \text{H}_2 + \text{CH}_3$
2. $\text{CH}_4 + \text{OH} \rightleftharpoons \text{H}_2\text{O} + \text{CH}_3$

Methyl reactions

3. $\text{CH}_3 + \text{O} \rightleftharpoons \text{CH}_2\text{O} + \text{H}$
4. $\text{CH}_3 + \text{OH} \rightleftharpoons \text{CH}_2\text{O} + 2\text{H}$
5. $\text{CH}_3 + \text{OH} \rightleftharpoons \text{CH}_2\text{O} + \text{H}_2$
6. $\text{CH}_3 + \text{H} \rightleftharpoons \text{CH}_4$
7. $\text{CH}_3 + \text{H} \rightleftharpoons \text{CH}_2 + \text{H}_2$
8. $\text{CH}_3 + \text{OH} \rightleftharpoons \text{CH}_2 + \text{H}_2\text{O}$

Formaldehyde reactions

9. $\text{CH}_2\text{O} + \text{H} \Rightarrow \text{CHO} + \text{H}_2$
10. $\text{CH}_2\text{O} + \text{OH} \Rightarrow \text{CHO} + \text{H}_2\text{O}$

Formyl Reactions

11. $\text{CHO} + \text{H} \Rightarrow \text{CO} + \text{H}_2$
12. $\text{CHO} + \text{OH} \Rightarrow \text{CO} + \text{H}_2\text{O}$
13. $\text{CHO} + \text{O}_2 \Rightarrow \text{CO} + \text{HO}_2$
14. $\text{CHO} + \text{M} \Rightarrow \text{CO} + \text{H} + \text{M}$

Methylene reactions

15. $\text{CH}_2 + \text{O}_2 \Rightarrow \text{CO}_2 + \text{H}_2$
16. $\text{CH}_2 + \text{O}_2 \Rightarrow \text{CO} + \text{OH} + \text{H}$
17. $\text{CH}_2 + \text{H} \Rightarrow \text{CH} + \text{H}_2$
18. $\text{CH}_2 + \text{OH} \Rightarrow \text{CH}_2\text{O} + \text{H}$
19. $\text{CH}_2 + \text{OH} \Rightarrow \text{CH} + \text{H}_2\text{O}$

Methylidyne reactions

19. $\text{CH} + \text{O}_2 \Rightarrow \text{CHO} + \text{O}$
20. $\text{CH} + \text{OH} \Rightarrow \text{CH}_2\text{O} + \text{H}$

H₂O₂ chemistry

21. $\text{H} + \text{O}_2 \rightleftharpoons \text{OH} + \text{O}$
22. $\text{H}_2 + \text{O} \rightleftharpoons \text{OH} + \text{H}$
23. $\text{H}_2 + \text{OH} \rightleftharpoons \text{H}_2\text{O} + \text{H}$
24. $\text{H}_2\text{O} + \text{O} \rightleftharpoons 2\text{OH}$

Hydroperoxyl formation/consumption

25. $\text{H} + \text{O}_2 + \text{M} \Rightarrow \text{HO}_2 + \text{M}$
26. $\text{HO}_2 + \text{H} \Rightarrow 2 \text{OH}$
27. $\text{HO}_2 + \text{H} \Rightarrow \text{H}_2 + \text{O}_2$
28. $\text{HO}_2 + \text{H} \Rightarrow \text{H}_2\text{O} + \text{O}$
29. $\text{HO}_2 + \text{OH} \Rightarrow \text{O}_2 + \text{H}_2\text{O}$

TERMINATION

30. $\text{CO} + \text{OH} \Rightarrow \text{CO}_2 + \text{H}$



Conversion to products by sequential fragmentation by elementary reactions (H atom abstraction)

Chemical Kinetics IVPs

Chemical kinetics IVPs in adiabatic environments

- For an arbitrary reaction mechanism,

$$\sum_{i=1}^{n_s} v'_{k,i} M_i \rightleftharpoons \sum_{i=1}^{n_s} v''_{k,i} M_i, \quad k = 1, \dots, n_r$$

- Mass conservation:

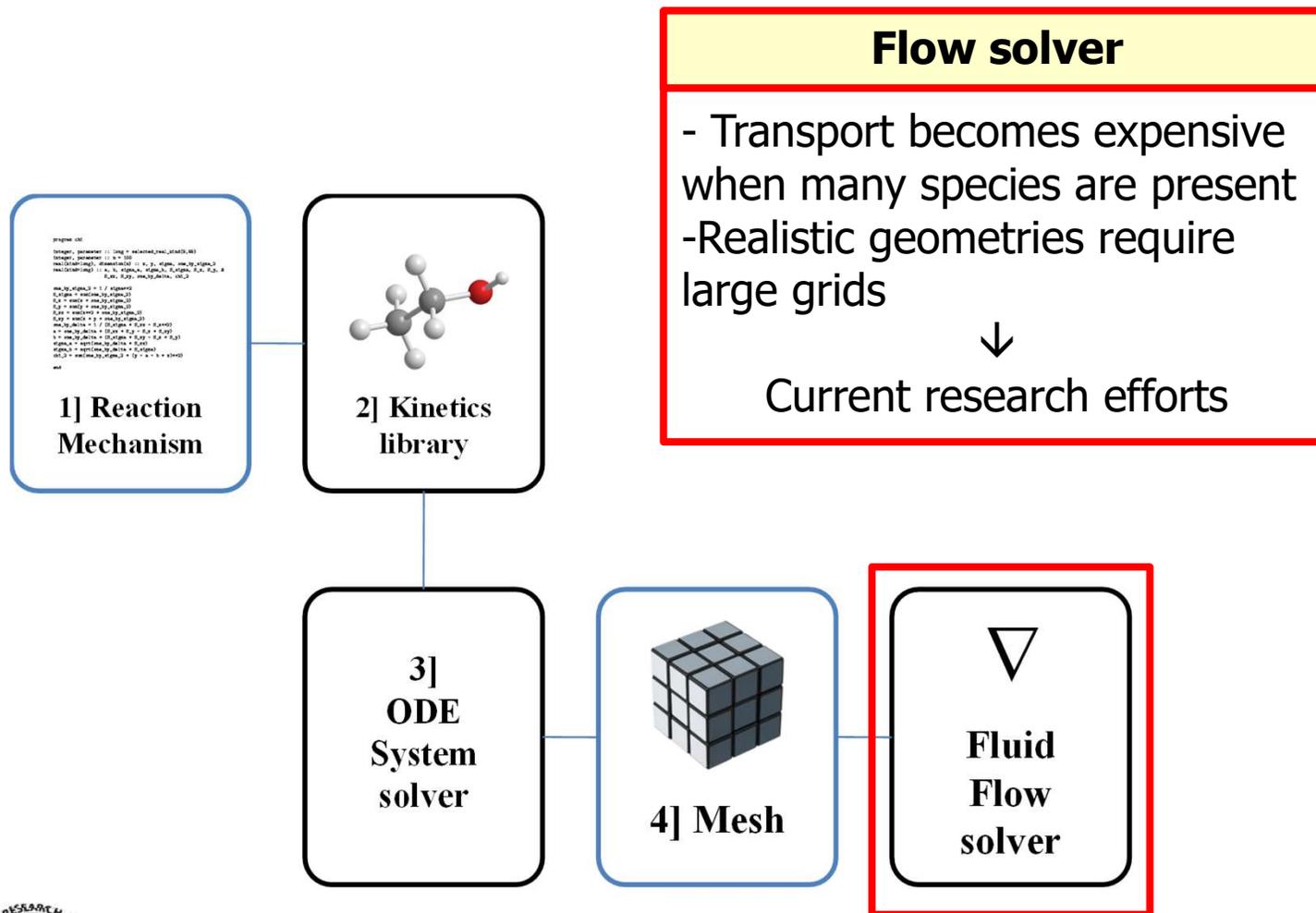
$$\frac{dY_i}{dt} = \frac{W_i}{\rho} \sum_{k=1}^{n_r} (v''_{k,i} - v'_{k,i}) q_k(\mathbf{Y}, T), \quad i = 1, \dots, n_s$$

- Energy conservation:

$$\frac{dT}{dt}(\mathbf{Y}, T) = -\frac{1}{\bar{c}_v(\mathbf{Y}, T)} \sum_{i=1}^{n_s} \left(\frac{U_i(T)}{W_i} \frac{dY_i}{dt}(\mathbf{Y}, T) \right)$$

- Integrated with stiff ODE solvers (VODE, LSODE, RADAU5...)
- Only species and internal energy sources are linked to the CFD solver

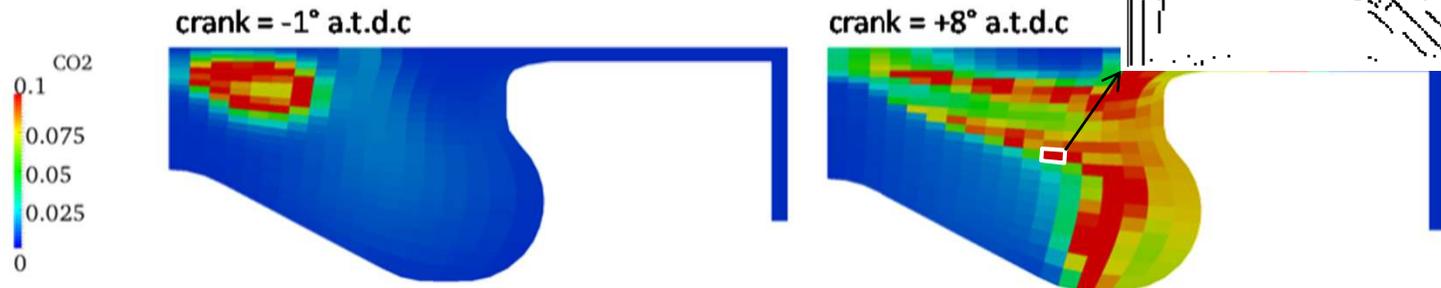
Two levels of interaction



Potential for speed-up

ODE system level (1 reactor) →

finite volume domain level (N reactors) ↓



- When/where does chemistry need to be solved in a computational domain?
- Is it worthwhile to solve it in each single cell?
- On which basis can reacting cells be regarded as 'similar' or 'different'?

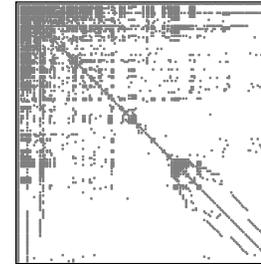
Mechanism size and sparsity

Perini, 2012

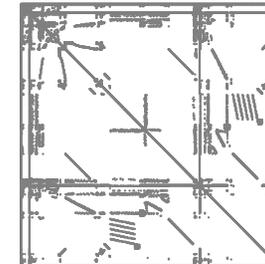
Sparsity of hydrocarbon fuel mechanisms increases with size



47 (62.7%)



160 (86.2%)

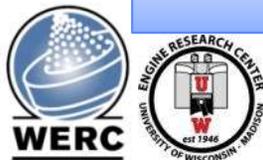
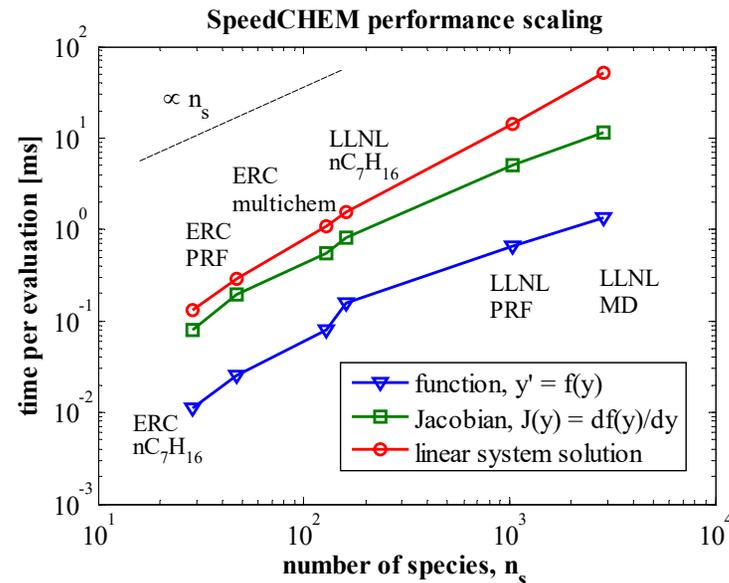


2878 (99.7%)

n_s

- All the functions and equations are evaluated in matrix form
- ODE system function, analytical Jacobian evaluation and linear system solution achieve

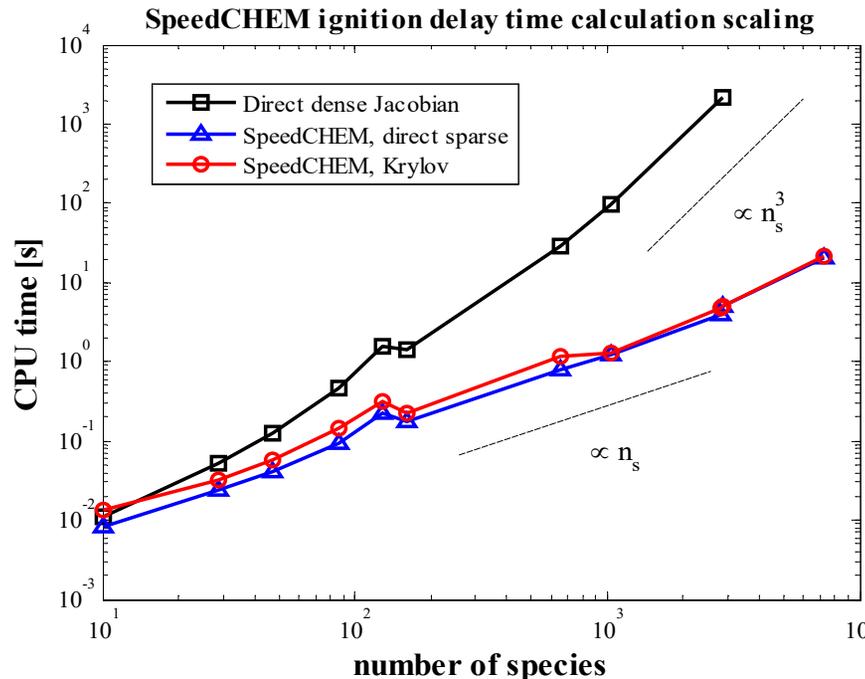
linear scaling with n_s



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Constant-volume reactor performance

Perini, 2014



9 reaction mechanism tested

- $n_s = 29$ to 7171

- $n_r = 52$ to 31669

18 ignition delay calculations per mech

- $\phi = [0.5, 1.0, 2.0]$

- $T_0 = [650, 800, 1000]$ K

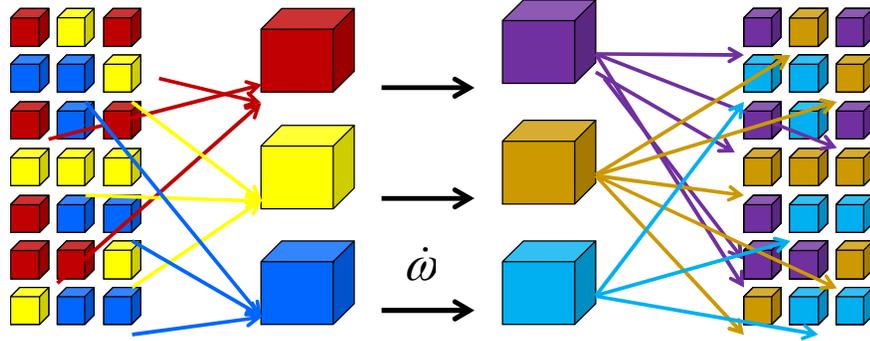
- $p_0 = [20, 50]$ bar

- $t = [0.1]$ s

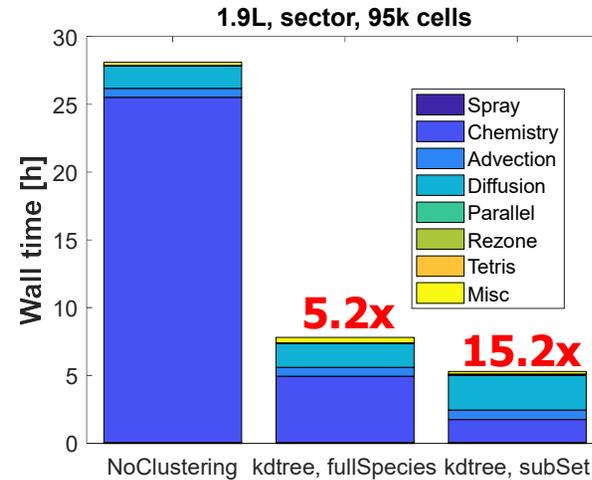
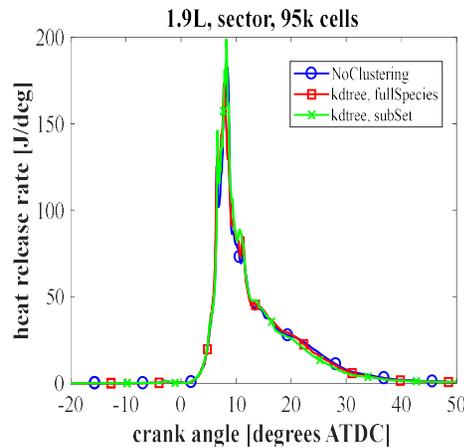
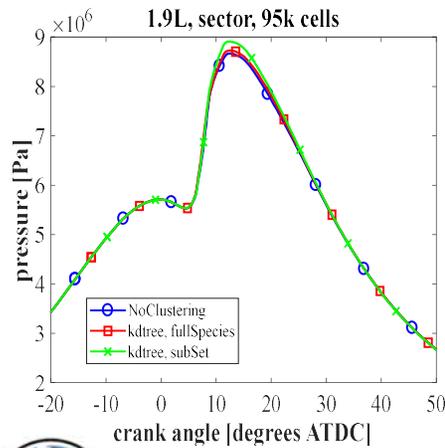
▪ Promising, efficient approach for practical engine simulations

1. Numerically exact solution (no mechanism reduction or manipulation).
2. Speed-up of more than three orders of magnitude at large sizes ($n_s > 1000$)
3. Even for modest sizes (~50-500 species), overall CPU time for chemistry is reduced by 3-10 times in comparison with dense chemistry integrators
4. Preconditioned Krylov solution for future, very large mechanisms

On-the-fly HD cell clustering

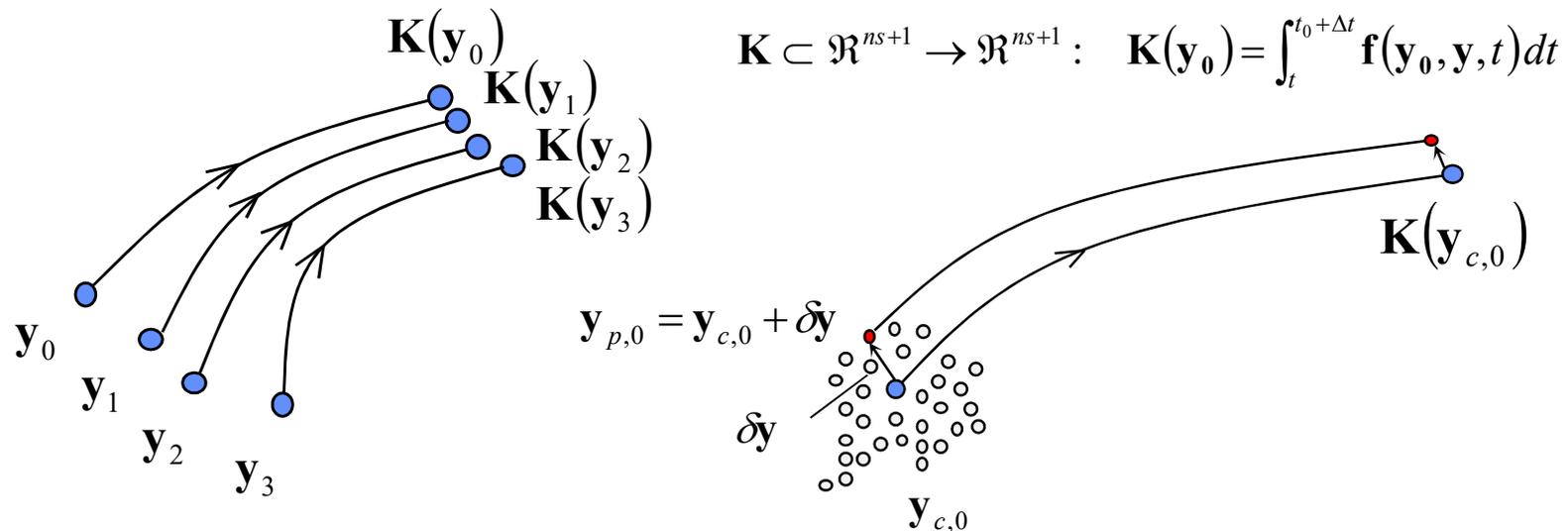


- No expensive storage/retrieval
- Unlimited number of clustering dimensions
- Intrinsic optimal cluster partition definition
- HD Kd-tree partitioning + NN-constrained k-means



Mapping function linearization

- Knowing the solution at the cluster center, we can extrapolate a solution for each of its individual members



$$\mathbf{K}(\mathbf{y}_{p,0}) \approx \mathbf{K}(\mathbf{y}_{c,0}) + \left. \frac{\partial K_i}{\partial y_j} \right|_{y=\mathbf{y}_{c,0}} \delta \mathbf{y}$$

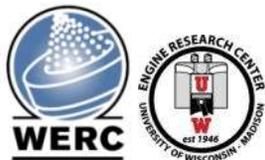
Perini & Reitz,
FCOMP 2015

Matrix of linearized mapping gradients



Multi-physics models for engines

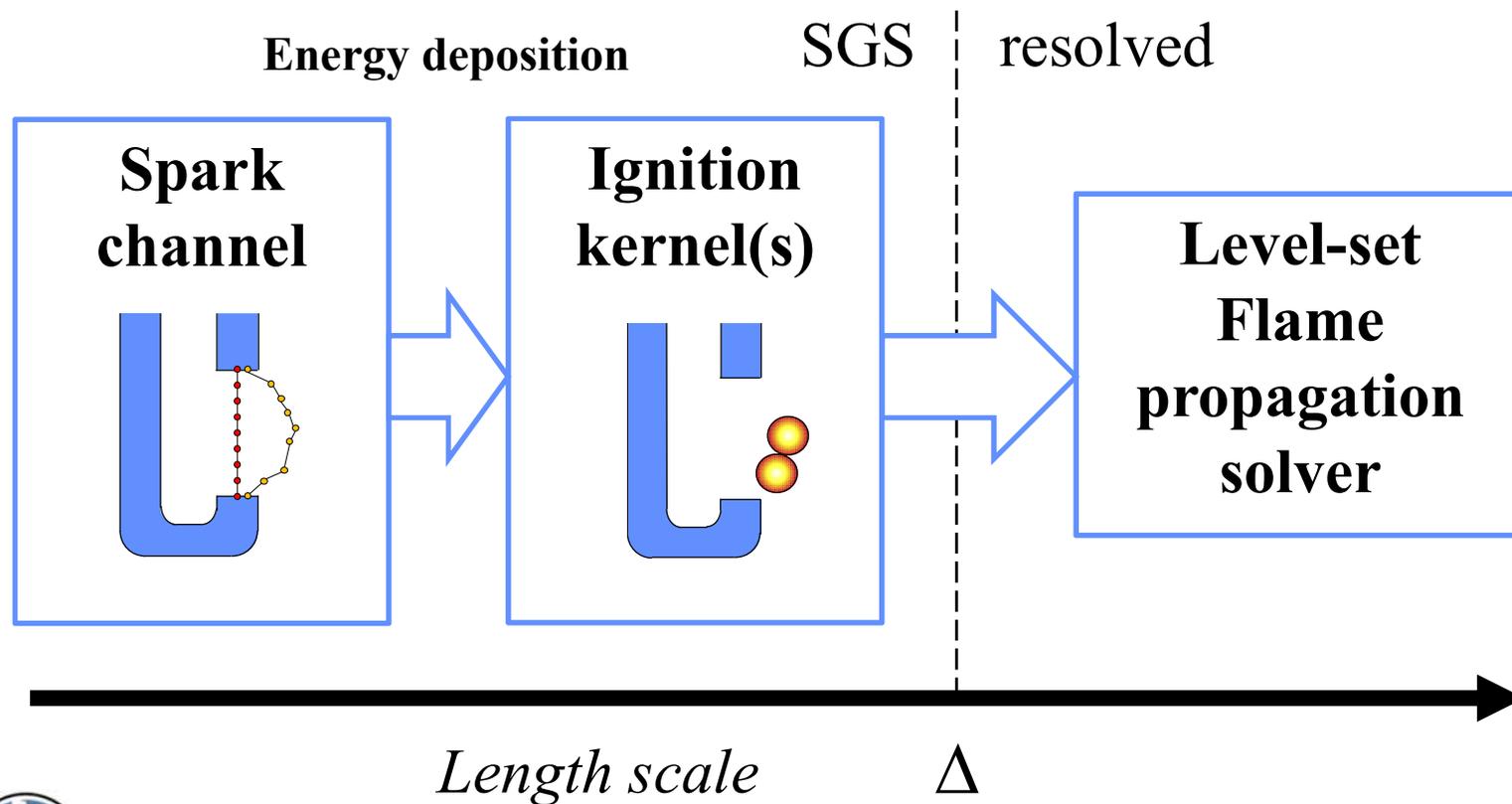
Ignition and flame propagation



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Ignition kernel and flame propagation modelling

- The spark plug and ignition kernel(s) have smaller time and spatial scales than typical grid sizes



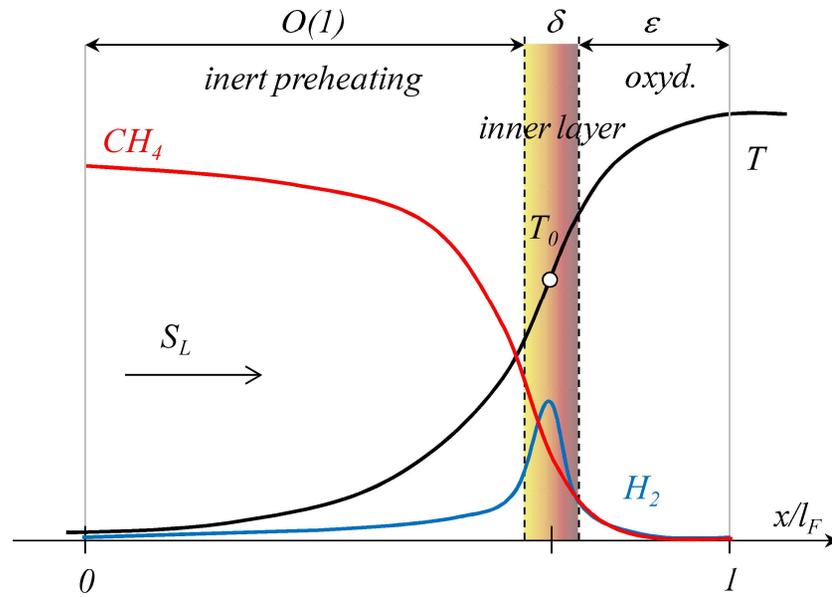
G-Equation model

Peters, 2000

Tan, 2003

Liang, 2006

- Widely used *level-set* method for the wrinkled flamelet regimes



In corrugated-flamelet & thin-reaction-zone regimes, eddies below Kolmogorov scale do not enter the inner layer

Inner flame layer modeled as two-dimensional, faceted interface ruled by a transport equation:

Favre-averaged formulation solved on a node-centered level set field:

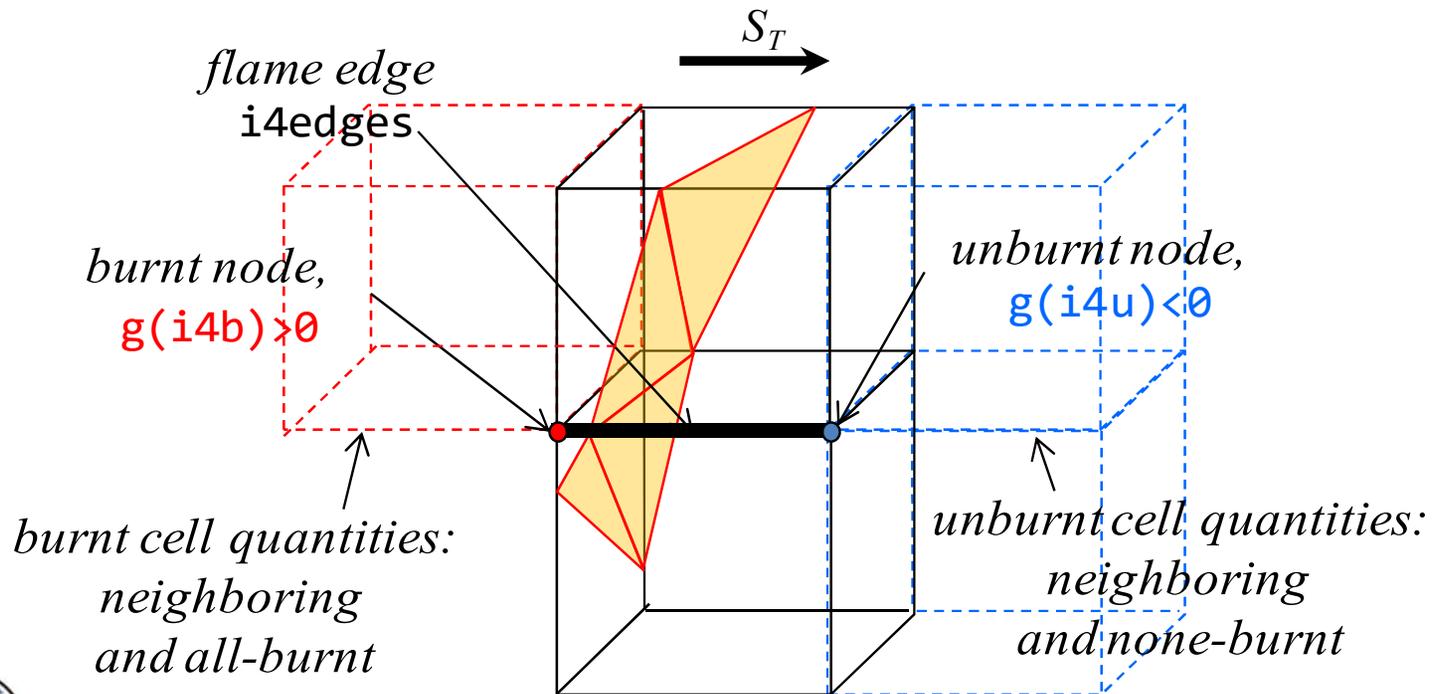
$$\frac{\partial G}{\partial t} + \mathbf{u} \cdot \nabla G = \frac{\rho_u}{\rho} S_T^0 |\nabla G| - D_T \kappa |\nabla G|$$



Numerical solution procedure – level-set

A level-set field represents the (signed) distance from an iso-surface

$$\frac{\partial G}{\partial t} + \mathbf{u} \cdot \nabla G = \frac{\rho_u}{\rho} S_T^0 |\nabla G| - D_T \kappa |\nabla G|$$



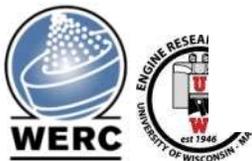
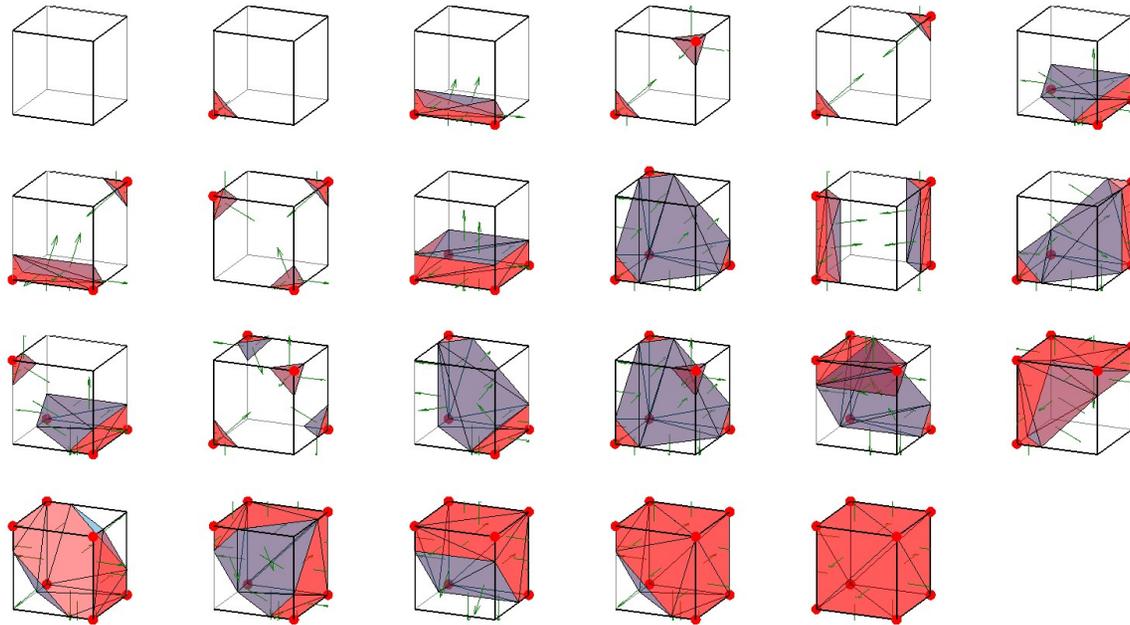
Swept-volume method for flame tracking

Flame surface areas and volumes can be tracked via a "marching cells" triangulation:

$$V = \frac{1}{3} \int_{\Omega} \nabla \cdot \mathbf{f} dV = \frac{1}{3} \int_{\partial\Omega} \mathbf{x} \cdot \hat{\mathbf{n}} dS = \dots = \frac{1}{3} \sum_{i=1}^{n_{tri}} A_i \mathbf{x}_{G,i} \cdot \hat{\mathbf{n}}_i$$

Triangles are planar: uniform normal

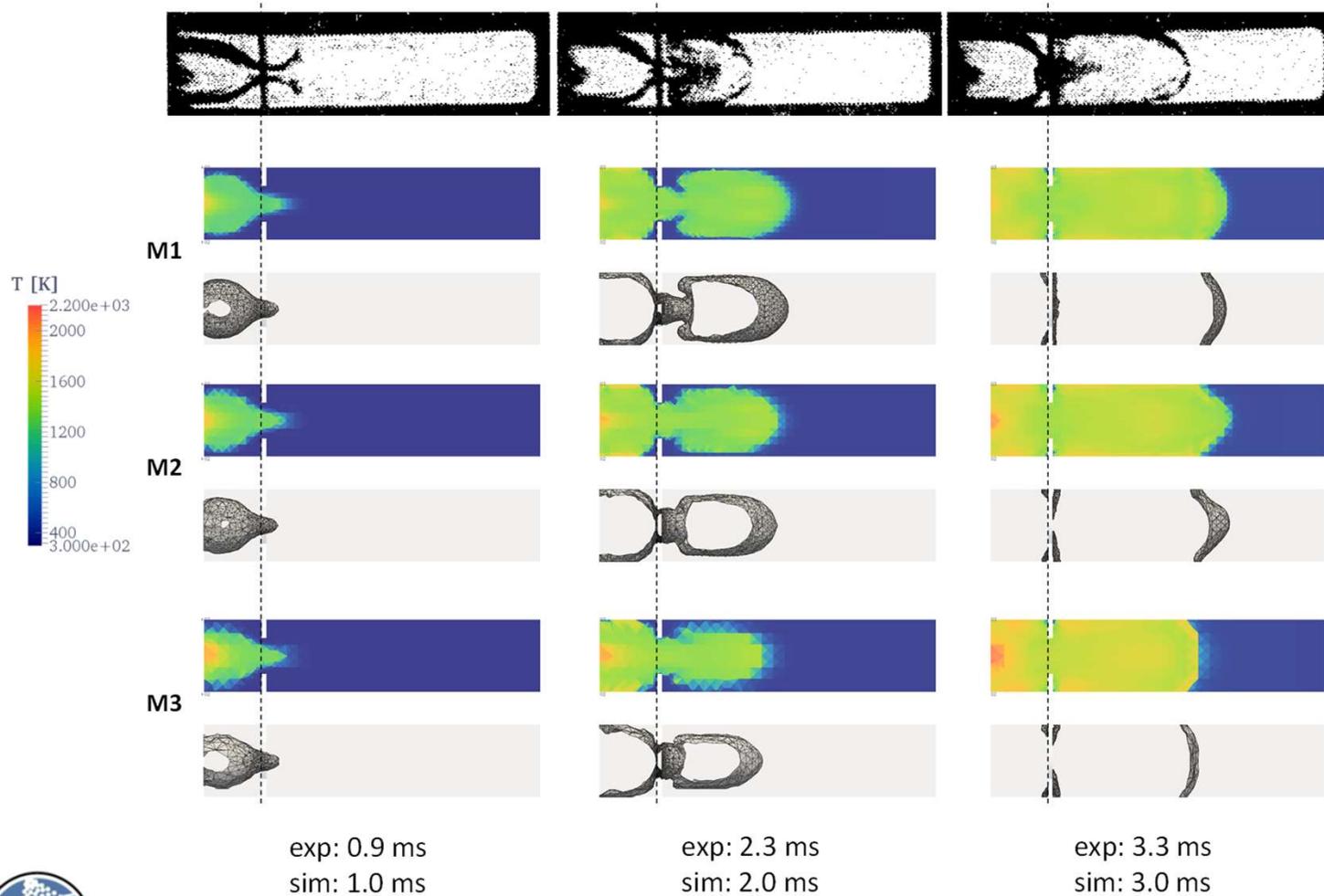
Definition of barycenter



Zhu, 2018 Perini, 2016

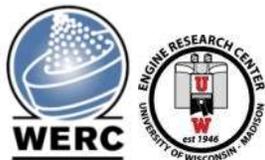
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Furukawa's chamber, $D = 15$ mm



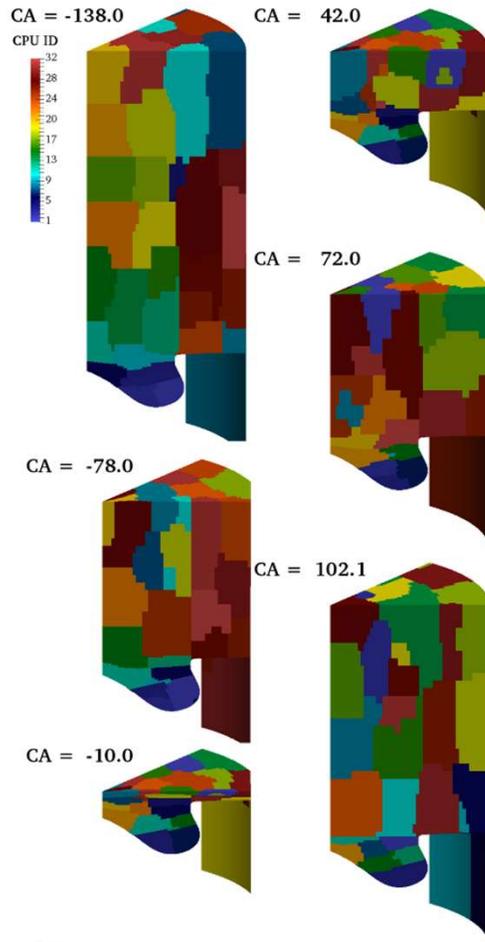
Capture flame propagation through orifices at sonic conditions

Multi-physics models for engines Computing



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Parallelism

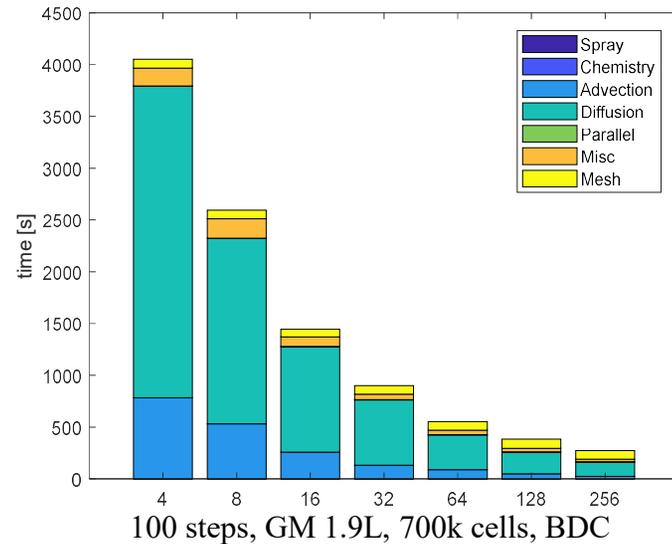
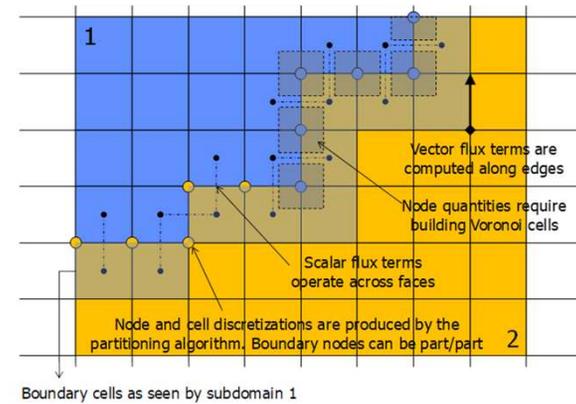


- ✓ Recursive domain decomposition
 - Arbitrary method (METIS, ParMETIS..)
 - Unstructured topology
 - Arbitrary accuracy

- ✓ Nonblocking comms

- ✓ On-the-fly update (Tetris, load)

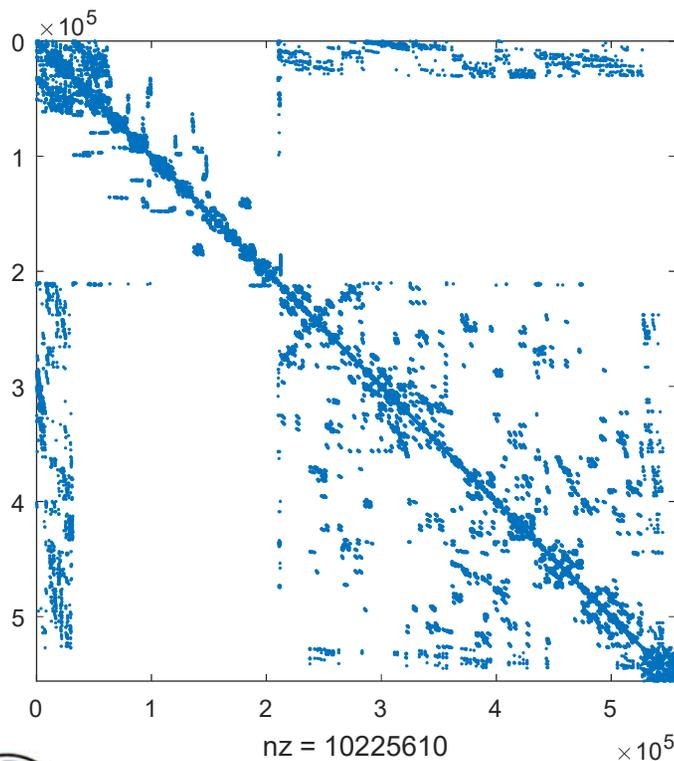
- ✓ Good scaling down to 3k cells/CPU



Finite-volume operators lead to large linear systems

$$\int_V \nabla^2 p \, dV = \int_S \nabla p \cdot \hat{n} \, dS = \sum_f \nabla p_f \cdot A_f = \mathbf{L} * p$$

“Laplacian”
matrix



- Linear systems can use up to 80% of the total CPU time
- To be solved in parallel using iterative Krylov solvers
- Suitable matrix preconditioners for optimal CPU vs. MPI trade-off



Perini, HPCEuropa3 project, 2018

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Conclusions/Outlook

- **Computer modelling (local->HPC->exascale) necessary to achieve combustion efficiency and pollutant emission goals**
- **Engine modelling is a strongly interdisciplinary challenge: energy, fluid dynamics, multiphase, chemistry, mathematics, computing, ...**
- **Significant work yet to be done to make combustion models more predictive, accurate, fast**



Thanks! Questions?

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Steve Busch, Paul Miles**



**University of Wisconsin
Advanced Computing Initiative**

